

Madison, Wisconsin

CITY OF MADISON CITY ENGINEERING DIVISION DEPARTMENT OF PUBLIC WORKS PLAN OF PROPOSED IMPROVEMENT

PROJECT

0709-242-0307-2 O'HERN, VINCENT

& LINDA 01 KING ST **LOCATION**

0709-242-0306-4 107 KING ST LLC 107 KING ST

INDEX OF SHEETS

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SHEET NO.	LI	LANDS	CAPE PLAN	V				
SHEET NO.	S1	PLAN	TER WALL	STRUCT	URE			

101 KING STREET – LUCILLE MADISON CITY PROJECT NO. 11836 CITY CONTRACT NO. 8159 MUNIS NO. 11836

> 0709-242-0303-0 MAJESTIC BUILDING LLC 115 KING ST

KING ST

0709-242-0301-4 106 E DOTY ST LLC 106 E DOTY ST

PLOT NAME:







TABLE 1806.2 PRESUMPTIVE LOAD-BEARING VALUES

	VERTICAL FOUNDATION	LATERAL BEARING	LATERAL SLIDING RESISTANCE		
CLASS OF MATERIALS	PRESSURE (psf)	(psf/ft below natural grade)	Coefficient of friction ^a	Cohesion (psf)b	
1. Crystalline bedrock	12,000	1,200	0.70		
2. Sedimentary and foliated rock	4,000	400	0.35	1000	
3. Sandy gravel and/or gravel (GW and GP)	3,000	200	0.35		
4. Sand, silty sand, clayey sand, silty gravel and clayey gravel (SW, SP, SM, SC, GM and GC)	2,000		0.25		
5. Clay, sandy clay, silty clay, clayey silt, silt and sandy silt (CL, ML, MH and CH)	1,500	100		130	
a. Coefficient to be multiplied by the dead load b. Cohesion value to be multiplied by the contr 1806.3 Lateral load resistance. Where the presumptive values of Tab	act area, as limited by Section 1806.3.2. le 1806.2 are used to determine	resistance to lateral loads, the c	alculations shall be in acco	rdance with Section	
1806.3.1 through 1806.3.4.					
The total resistance to lateral loads sliding resistance specified in Table	s shall be permitted to be determin a 1806.2.	ed by combining the values derive	d from the lateral bearing pre	essure and the late	
1806.3.2 Lateral sliding resistance	e limit.				
For clay, sandy clay, silty clay, clay	ey silt, silt and sandy silt, in no cas	e shall the lateral sliding resistance	e exceed one-half the dead lo	oad.	
1806.3.3 Increase for depth. The lateral bearing pressures spec to a maximum of 15 times the tabul	ified in Table 1806.2 shall be perm lar value.	nitted to be increased by the tabula	ar value for each additional fo	ot (305 mm) of dep	
1806.3.4 Increase for poles.			K		
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solated poles for uses such as flagpoles or signs and poles used to support buildings that are not adversely a (100000) a 12-inst N2. mm) motion at ground surface due to short-term lateral loads shall be permitted to be designed using lateral bearing pressure equal to two times the tabular values.

1607.8 Loads on handrails, guards, grab bars, seats and vehicle barriers.

Handrails, guards, grab bars, accessible seats, accessible benches and vehicle barriers shall be designed and constructed for the structural loading conditions set forth in this section.

1607.8.1 Handrails and guards.

Handrails and guards shall be designed to resist a linear load of 50 pounds per linear foot (plf) (0.73 kN/m) in accordance with Section 4.5.1 of ASCE 7. Glass handrail assemblies and guards shall also comply with Section 2407.

Exceptions

1. For one- and two-family dwellings, only the single concentrated load required by Section 1607.8.1.1 shall be applied.

2. In Group I-3, F, H and S occupancies, for areas that are not accessible to the general public and that have an occupant load less than 50, the minimum load shall be 20 pounds per foot (0.29 kW/p)

1607.8.1.1 Concentrated load.

Handrails and guards shall be designed to resist a concentrated load of 200 pounds (0.89 kN) in accordance with Section 4.5.1 of ASCE 7.

Intermediate rails (all those except the handrail), balusters and panel fillers shall be designed to resist a concentrated load of 50 pounds (0.22 kN) in accordance with Section 4.5.1 of ASCE 7.







TORSION ON BEAM

CLOSED WITH 135 DEGREE BEND

> Tu = 1.6(1000)(3.5') = 5600 FT-LBS Vu = 1.6(1000)/2 = 800 LBS bw = 12" d = 24"-4" = 20" ph = 6+6+18+18 = 48 Aoh = 0.85*Ao = 0.85*108 = 91.8 IN^2 $Vc = 2(f'c)^{1/2} bw^*d = 26290 LBS$ PHI = 0.65

[(Vu/bw*d)^2+(Tu*ph/1.7 Aoh^2)^2]^1/2 <= PHI (Vc/bw*d)+8(f'c)^1/2

19.1 <= 356 THEREFORE OK FOR TORSION

SEE BEAM CALC ON FOLLOWING PAGES

